

New Scientist Magazine - Aug. 1999

Solitary Killers - "The sea was calm when two friends took their boat out for a quiet spot of fishing. In the distance, a high-speed catamaran passed them. Ten minutes later, a huge wave 5m high came out of nowhere and swamped their 11m boat. Sibley was thrown overboard and drowned. Hayman later told reporters that the wave looked like the white cliffs of Dover"

Complaints - Ship-Generated Waves

- Bank stability and shoreline erosion
- Potential impact on marine life in coastal wetlands
- Risk to smaller boats using waterways
- Swimmer safety
- Berthing/mooring and On-Offloading difficulties for cargo vessels in inland ports
- Hazard to recreational boat marinas

New-Generation Vessels

- High-Speed Vessels
 - Speeds of 35 to 50 knots compared to 10 to 15 knots for conventional vessels
- Deep Draft Vessels
 - Post-Panamax
 Class of Vessels
 - Length=O(1000ft), Beam=O(150ft), Draft = O(50ft)

Modeling Approaches

- Far-Field
 - Shallow Water
 Equations
 - Boussinesq
 Equations

- Near-Field
 - Boundary-Integral Methods
 - Navier-Stokes
 Equations

Far-Field Methods

Shallow Water Equations

- hydrostatic pressure
- nondispersive waves
- better suited for estimating water level drawdown/return currents

Boussinesq Equations

- non-hydrostatic pressure
- able to deal with shorter-period dispersive waves
- poor description of flow field around ship hull compared to near-field methods

Near-Field Methods

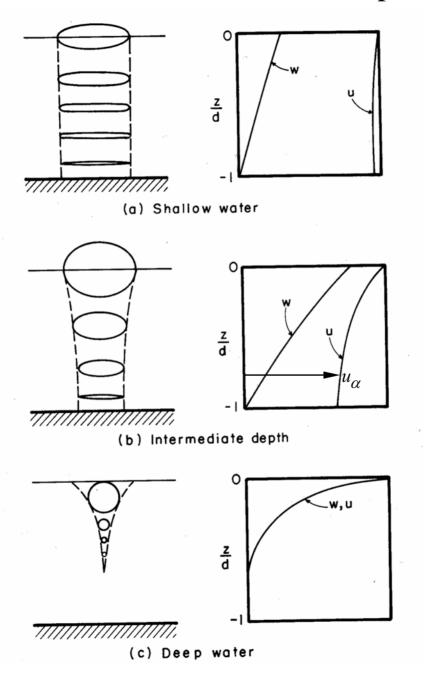
Boundary-Integral Methods

- assumes irrotational flow
- accurate description of flow around ship
- computationally intensive for large areas when you have to discretize seabed in addition to body and free surface

Navier-Stokes Equations

- able to deal with viscous effects
- accurate description of flow around ship
- computationally intensive for large areas

Wave Orbital Variation with Depth



Boussinesq Equations

• Taylor series expansion of velocity potential around arbitrary elevation z_{α} in water column

$$\Phi(x, y, z, t) = \phi_{\alpha}(x, y, t) + (z_{\alpha} - z)\nabla \bullet (h\nabla \phi_{\alpha}) + \frac{1}{2}(z_{\alpha}^{2} - z^{2})\nabla^{2}\phi_{\alpha}$$

- quadratic variation for horizontal velocities and hydrodynamic pressure
- linear variation for vertical velocity
- substitute into 3-D mass and momentum equations and integrate over depth

Boussinesq Equations

Mass Conservation Equation

$$\eta_t + \nabla \cdot \mathbf{Q} = 0, \quad \text{where} \quad \mathbf{Q} = \int_{-h}^{\eta} u \, dz$$

Momentum Equation

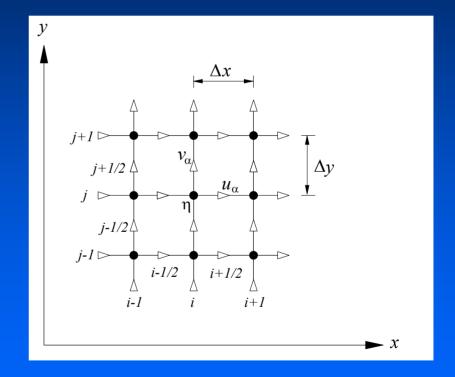
$$\mathbf{u}_{\alpha,t} + g\nabla \eta + (\mathbf{u}_{\alpha} \cdot \nabla)\mathbf{u}_{\alpha} + \left[\frac{z_{\alpha}^{2}}{2}\nabla(\nabla \cdot \mathbf{u}_{\alpha,t}) + z_{\alpha}\nabla[\nabla \cdot (h\mathbf{u}_{\alpha,t})]\right] = 0$$

Ship represented by line source (Tuck, 1966)

$$\left. \overline{v} \right|_{y=0} = \pm \frac{U_s}{2h} A_x$$

Numerical Solution

- Time-domain, finite difference method (modified Crank-Nicolson)
- Staggered Grid
- Line by line technique for momentum equations resulting in tridiagonal matrices for u_α, v_α



Practical Limitations

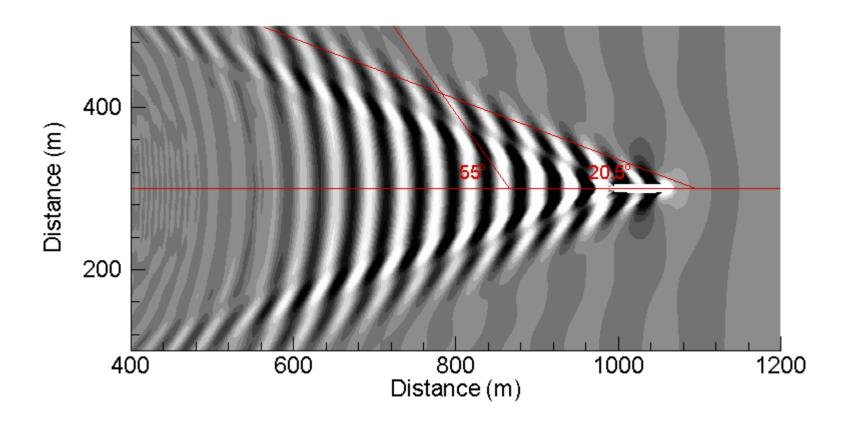
- Dispersive Limit
 - \blacksquare Water Depth/Wavelength, $h/L \le 0.5$
 - $\blacksquare Depth-based\ Froude\ Number,\ F_{nh}>0.65$
- Wavelength/Grid Size, $L/\Delta x > 10$
- Wave Period/Time Step Size, $T/\Delta t > 10$
- Courant Number for Numerical Stability

$$C_r = \sqrt{\left[C^2 \Delta t^2 \left(\frac{1}{\Delta x^2} + \frac{1}{\Delta y^2}\right)\right]} < 1$$

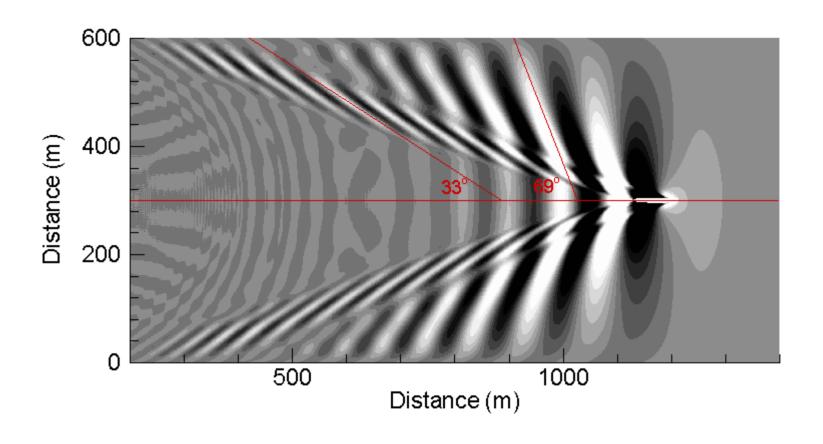
Characteristics of Ship-Generated Waves in Shallow Water

- Different flow regimes depending on depth based Froude Number ($F_{nh} = U_s/\sqrt{gh}$)
 - Subcritical regime $(F_{nh} < 1)$
 - Transcritical regime $(F_{nh} \approx 1)$
 - Supercritical regime $(F_{nh} > 1)$

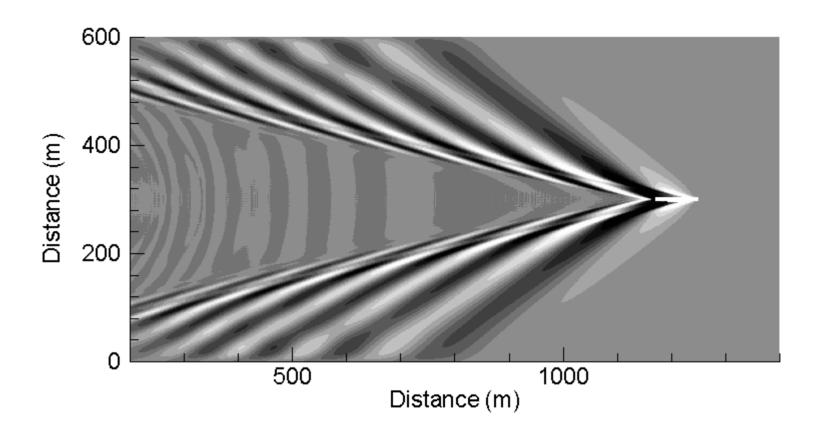
Instantaneous Water Surface Elevation for Ship Moving at Subcritical Speed ($F_{nh} = 0.65$)



Instantaneous Water Surface Elevation for Ship Moving at Transcritical Speed ($F_{nh} = 0.9$)



Instantaneous Water Surface Elevation for Ship Moving at Supercritical Speed ($F_{nh} = 1.5$)





High-Speed Vessel Waves

- Longer Periods (T = 9.5s for 35knots compared to 4.2s for 15knots)
 - Swell-type waves
 - Strongly affected by bathymetry/topography of channels
 - May not be visible until shoal and break in shallow water
 - Different breaking wave type (Plunging)

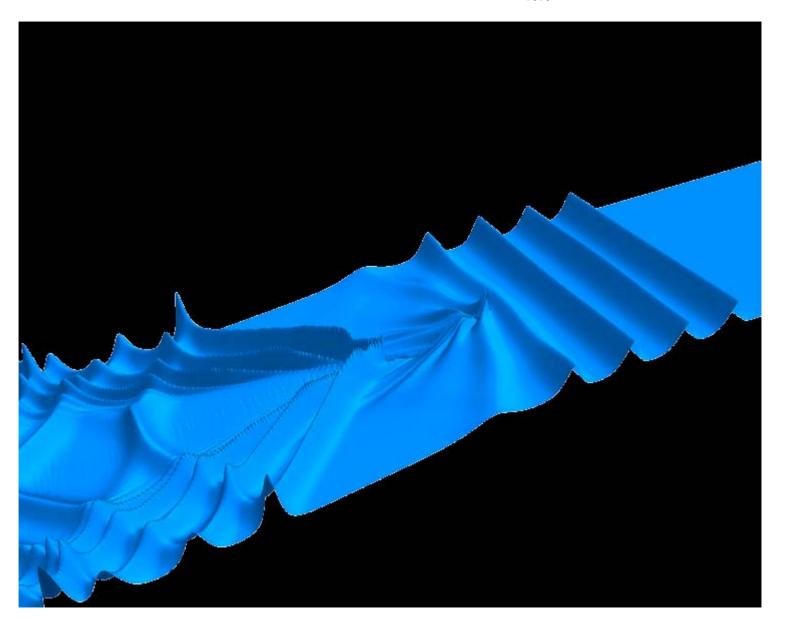
Generation of Upstream-Advancing Solitary Waves

- Occur at transcritical speeds $(F_{nh} = 1)$
- Initial observation by Sir John Scott Russell (1834) in a canal
- Maintain shape by balance between nonlinear and dispersive effects
- Wave breaking and transition to bores at supercritical speeds

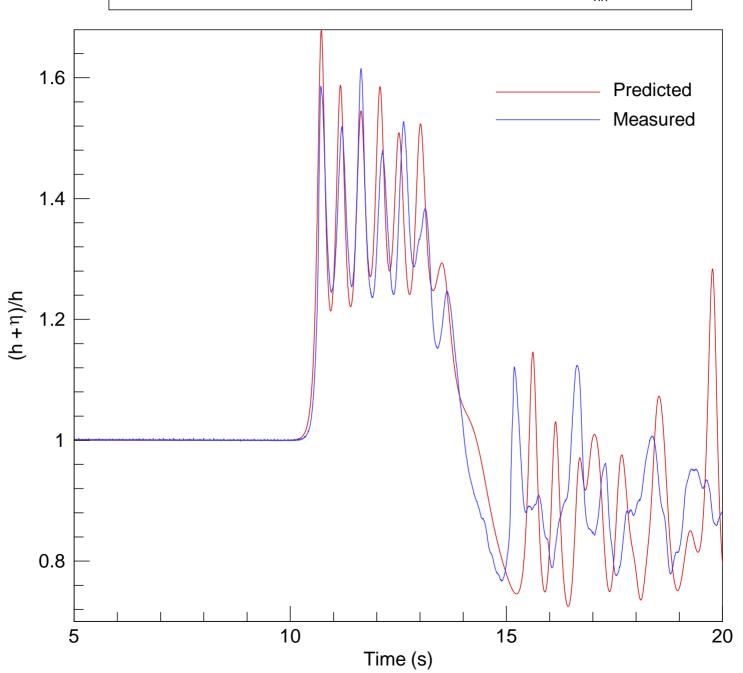
Laboratory Experiments – Gourlay (2001)

- 60-m long towing tank
- Tests with high-speed vessel (L=1.6m, B=0.4m, D=0.1m)
- Depth-based Froude numbers from 1.05 to 1.5

Upstream Solitary Waves $(F_{nh} = 1.10)$



Normalized Water Surface Elevation at x = 40m ($F_{nh} = 1.15$)



Deep-Draft Vessels in Navigation Channels

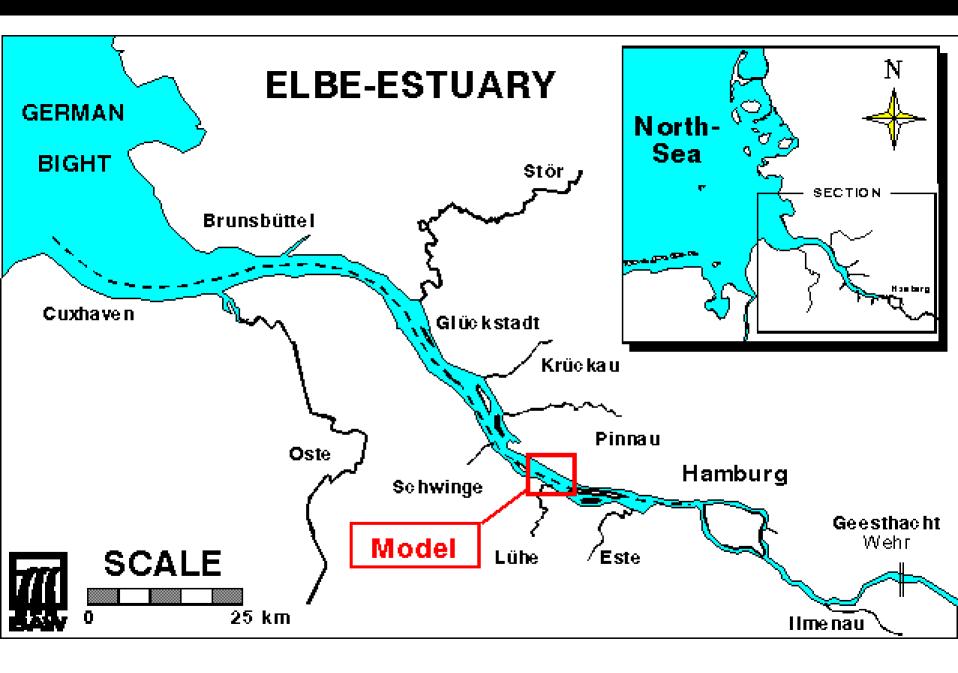
- Water Level Drawdown / Return Velocity in Confined Channels
- Underkeel Clearance (Squat / Vessel Motions)
- Generation of Surge Waves on Shallow Banks

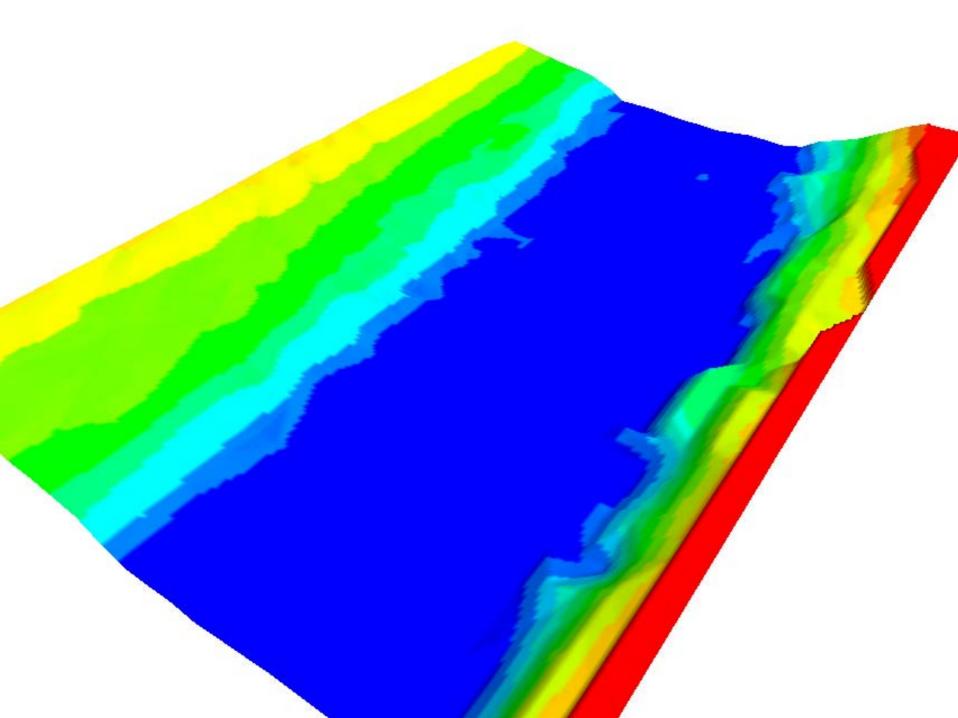
Water Level Drawdown and Return Currents in Confined Channels

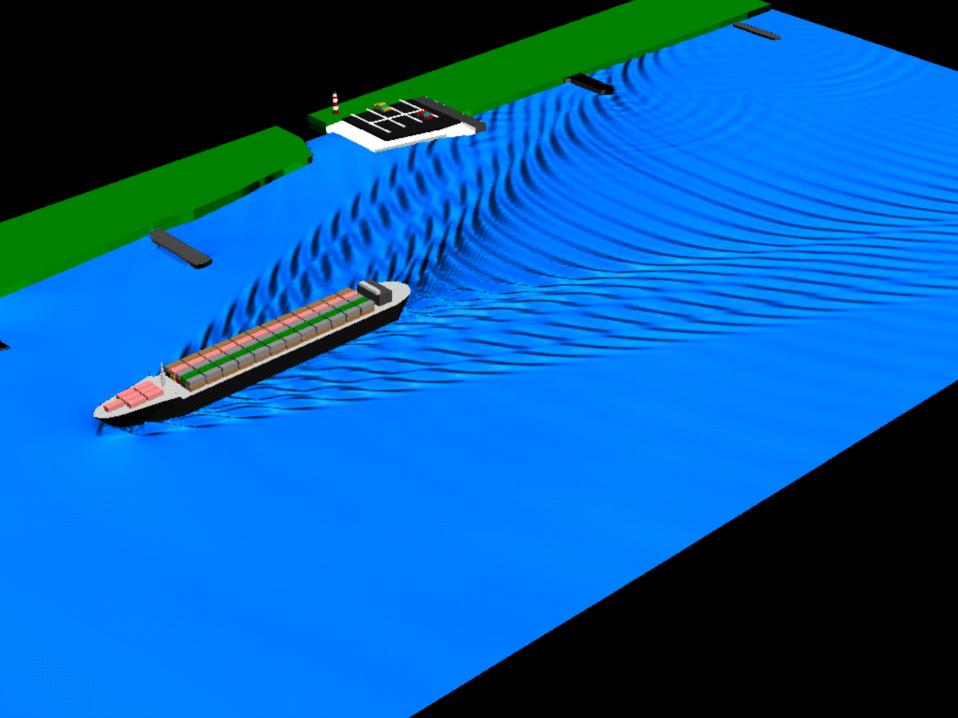
- 1-D Analytical Model Schijf (1949)
 - based on mass and energy conservation equations, does not consider across-channel variations in bottom topography or return currents
- Does not apply to 2-D waterways with side banks, structures, islands, etc

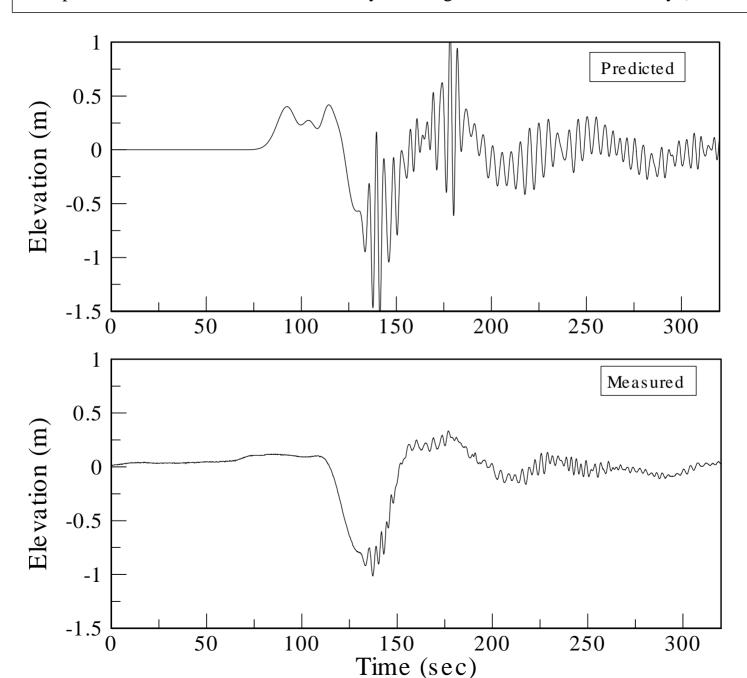
Elbe River Study

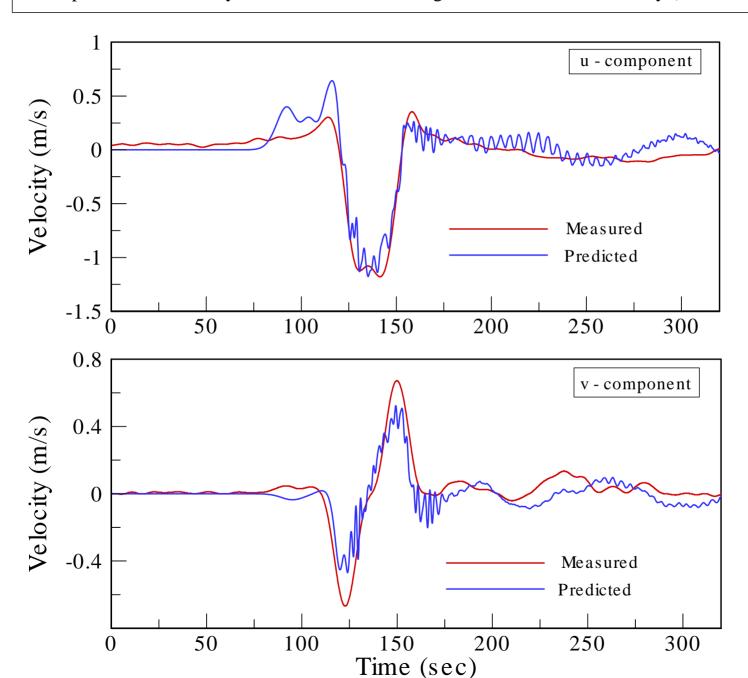
- 60000DWT Panamax Class Vessel
 - $\blacksquare Length = 280m$
 - $\blacksquare Beam = 32m$
 - Draft = 13.5m
- Ship Speeds (7 to 15 knots)
- 1:40 Physical Model Study at German Waterways Department











Mississippi River – Gulf Outlet (MRGO) Channel

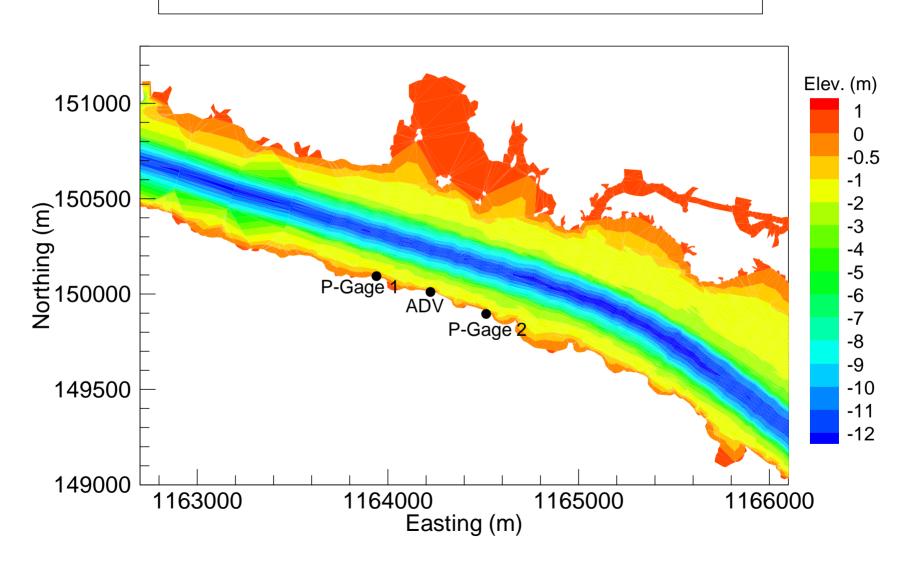
- 76 miles long, 500 ft wide and 40 ft deep
- Northern banks eroding at an average rate of 15 feet per year
- Considering use of articulated concrete mats to protect the channel banks

MRGO Field Experiments

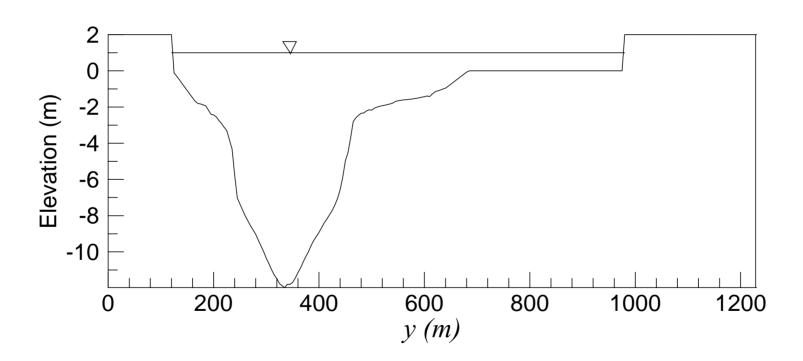
- Measurements: 30 May to 10 June 2002
- Four pressure gages
- Two Acoustic Doppler Velocimeters (ADVs)
- Deployed at two locations along channel banks (33000 ft apart)



North Site Bathymetry for MRGO Field Experiments



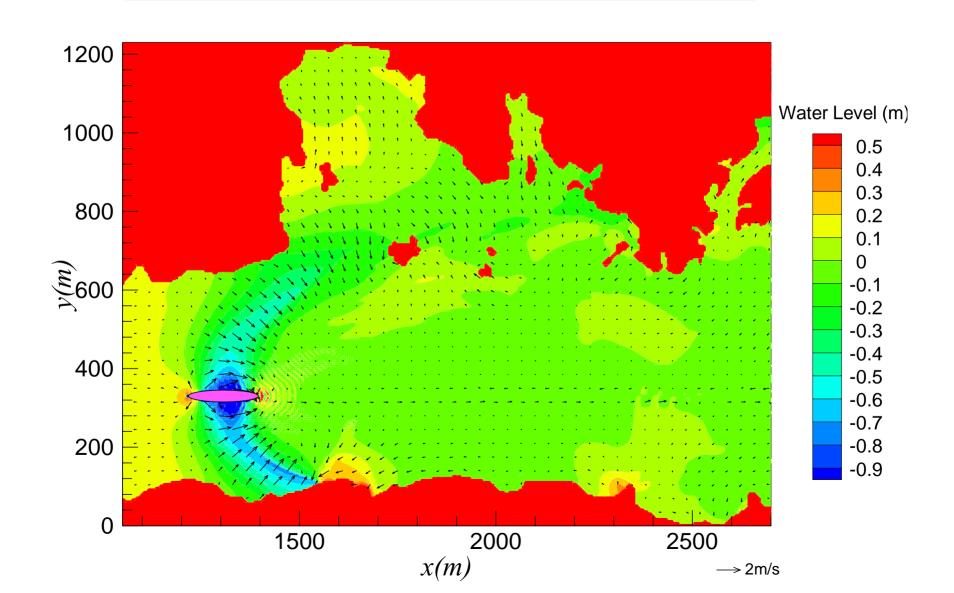
Across-Channel Transect at ADV (MRGO9) Location



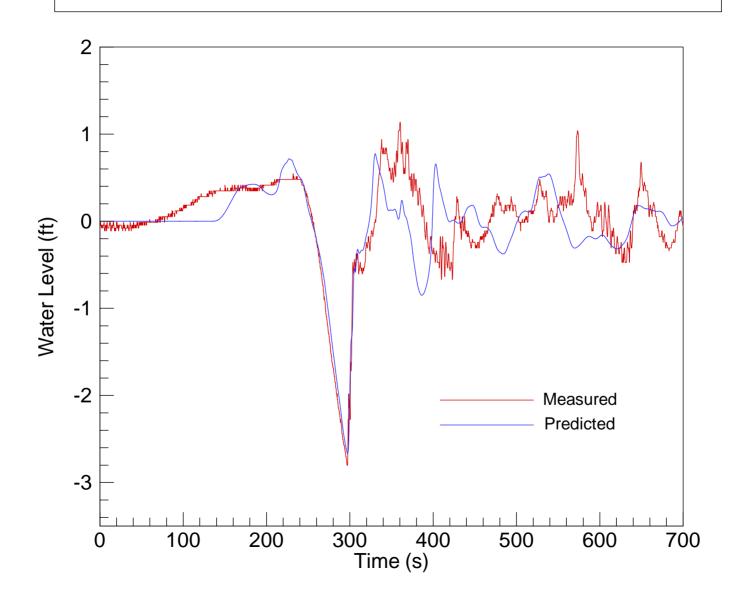
Sample Measured Data

- 5/30/02 at 21:00 hrs
 - Libra Buenos Aires (Length = 195m, Beam = 30m, Draft = 10m)
 - Estimated Ship Speed = 12knots
- 6/9/02 at 23:45 hrs
 - Lykes Commander (Length = 188m, Beam = 32m, Draft = 12.5m)
 - Estimated Ship Speed = 10knots

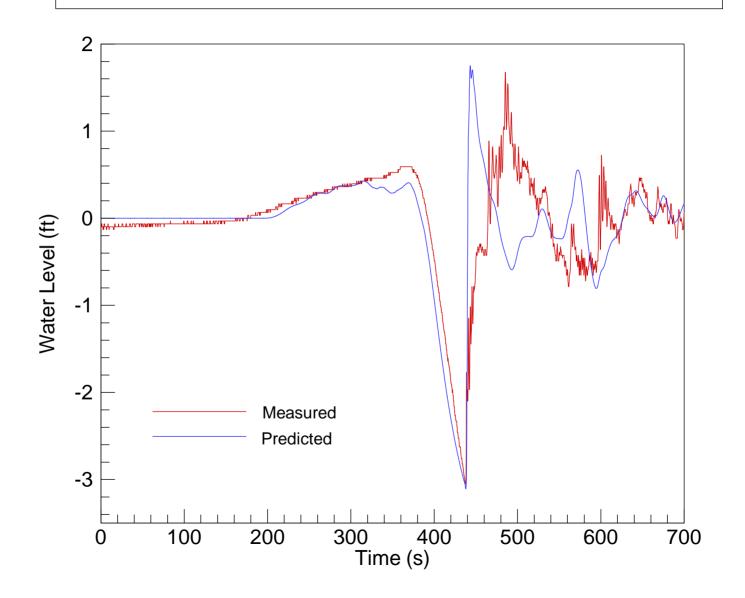
Ship-Induced Water Level and Flow Field Pattern (Inbound TMM Tabasco, $6/6/2002\ 04:10$, $U_s = 9.9\ knots$)



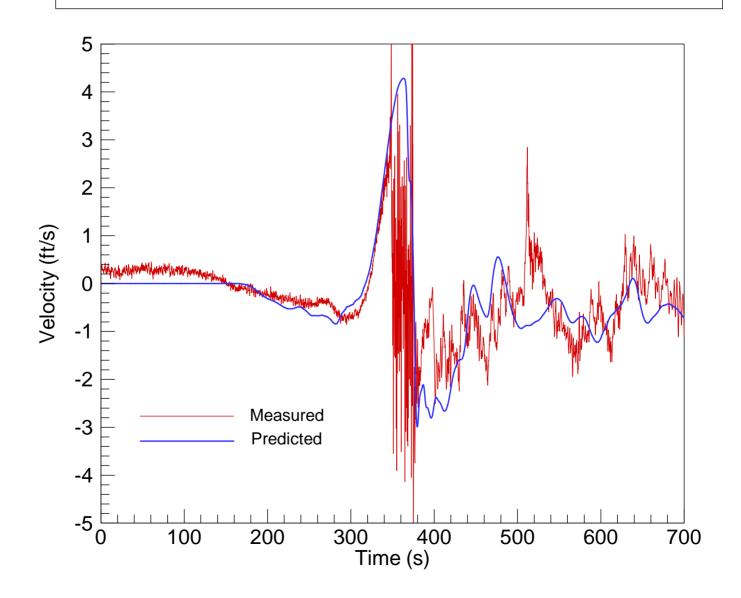
Comparison of Measured and Predicted Water Level Drawdown at 10509 (Inbound TMM Tabasco, 6/6/2002 04:10, $U_s = 9.9$ knots)



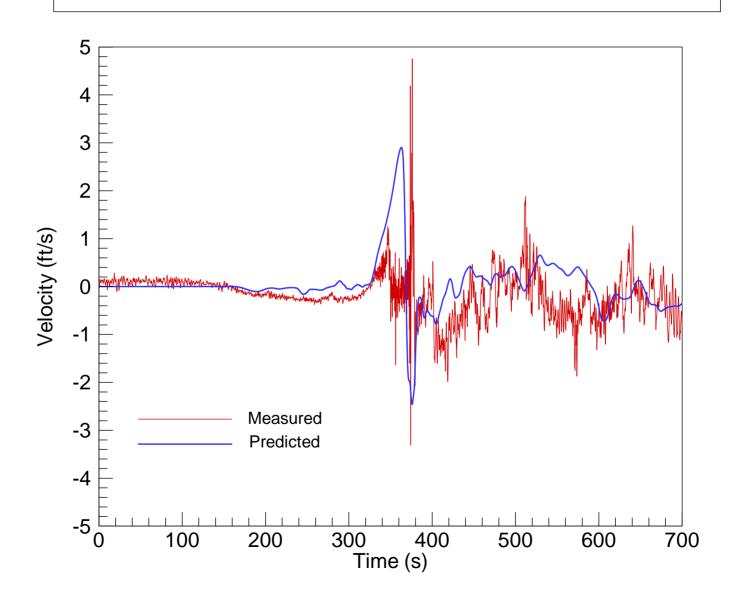
Comparison of Measured and Predicted Water Level Drawdown at 10508 (Inbound TMM Tabasco, 6/6/2002 04:10, $U_s = 9.9$ knots)



Comparison of Measured and Predicted Along-Channel Velocities (Inbound TMM Tabasco, $6/6/2002\ 04:10$, $U_s = 9.9\ knots$)



Comparison of Measured and Predicted Across-Channel Velocities (Inbound TMM Tabasco $6/6/2002\ 04:10,\ U_s=9.9\ knots)$



Concluding Remarks

- Boussinesq models are promising for investigating ship-generated waves in shallow water and their interaction with river banks and moored vessels
- Couple Boussinesq model with bank erosion and 6-dof vessel motion models
- Solve Boussinesq equations on unstructured grid using finite volume method